

# Analytical modeling of the evolution of the nonlinearity parameter of sensitized stainless steel.

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## Motivation

### Precipitation in Stainless Steel

- Stainless steels have a wide range of uses in the energy industry due to their corrosion resistance.
- When exposed to high temperatures, carbon and chromium diffuse to the grain boundary, forming  $M_{23}C_6$  carbides (sensitization).
- Chromium-depleted zones near the grain boundary become susceptible to corrosive attack, including stress corrosion cracking.

### Nonlinear Ultrasonic Techniques (NLU)

- NLU has been shown to be sensitive to sensitization in stainless steel.
- There are few models relating the acoustic nonlinearity parameter,  $\beta$ , to a quantified amount of damage in stainless steel.

## Objectives

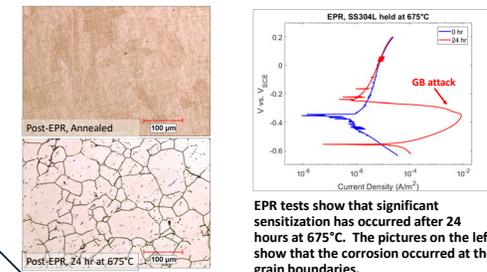
- Develop a diffusion model that accurately predicts  $M_{23}C_6$  precipitate growth in thermally aged stainless steel.
- Develop an analytical model relating  $M_{23}C_6$  growth to the increase in  $\beta$ .

## 304L Stainless Steel

SS 304L	C	Cr	Ni	Mn	Cu	Mo	Co
(wt %)	0.019	18.37	8.13	1.66	0.39	0.39	0.119

Bar samples: 6" x 2" x 0.75" (152 x 50.4 x 17.1 mm)

Heat Treatment: Annealing (1080°C, 30 min, Air Cool), followed by Sensitization @ 675°C, for 0 hr, 24 hr



EPR tests show that significant sensitization has occurred after 24 hours at 675°C. The pictures on the left show that the corrosion occurred at the grain boundaries.

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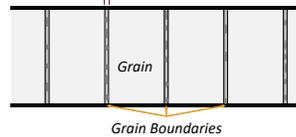
## Methods

### 1-D Grain Boundary Separation Model

Stress in the material is modeled as a 1-D series of distributed nonlinear springs, described by:

$$\text{Grain Boundary: } \sigma = k\epsilon_b + \frac{1}{2}k_2\epsilon_b \quad (1)$$

$$\text{Grain: } \sigma = E\epsilon_g + \frac{1}{2}E_2\epsilon_g \quad (2)$$



The acoustic nonlinearity parameter is given by:

$$\beta = \frac{\delta^2 \epsilon}{\delta \sigma^2} \left( \frac{\delta \epsilon}{\delta \sigma} \right)^{-2} \Big|_{\sigma=0} \quad (3)$$

Utilizing the relations described in (1) and (2), the contribution to the nonlinearity parameter from the grain,  $\beta_g$  and the grain boundary,  $\beta_b$ , are determined:

$$\beta_g = -\frac{E_2}{E} \quad (4)$$

$$\beta_b = \frac{r_0}{E} \left( \frac{2E_2}{k} - \frac{E_2^2 k_2}{k^3} \right) \quad (5)$$

We assume that grain boundary constants can be determined from a potential function, such as Lennard-Jones.

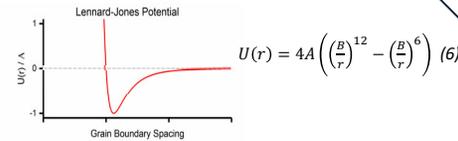
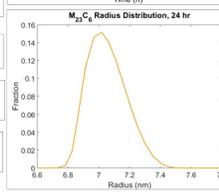
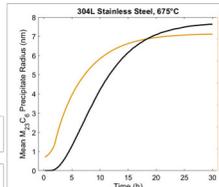
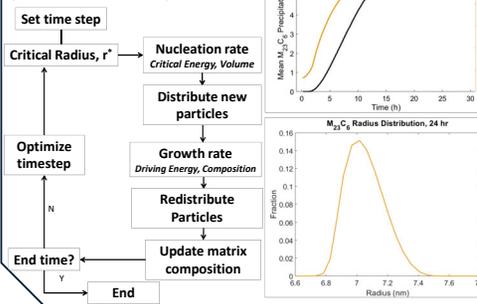
### Grain Boundary Precipitate Modeling

TC-PRISMA<sup>[4]</sup> Precipitate Growth Module (General) [J.-Y. Kim]

Assumptions

- Pseudo-steady state diffusion within each time step (based on matrix composition)
- $M_{23}C_6$  precipitates are spherical.

Based on Langer-Schwartz theory and Kampmann-Wagner numerical method to simulate nucleation, growth and coarsening



$$U(r) = 4A \left( \left( \frac{r_0}{r} \right)^{12} - \left( \frac{r_0}{r} \right)^6 \right) \quad (6)$$

$$k = \frac{r_0 \delta^2 U(r)}{\alpha^2 \delta r^2} \quad k_2 = \frac{r_0^3 \delta^3 U(r)}{\alpha^2 \delta r^3} \quad (7,8)$$

During thermal aging, grain-boundary precipitate radius grows:

$$r_p = r_0 (1 + \delta) \quad (9)$$

Under the assumption that  $r_0$  is the equilibrium spacing dictated by the Lennard-Jones potential, the relative change in  $\beta$  is then

$$\frac{\beta(r_p)}{\beta(r_0)} = 1 + \frac{56(1726a^2BE^2 + 54AE_2)\delta}{3(725a^2BE^2 + 48AE_2)} f \quad (10)$$

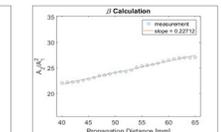
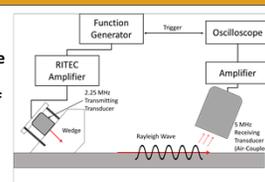
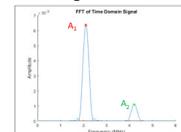
Given that the material properties are constants,  $\beta$  is then linearly related to the change in grain boundary thickness. In this work, we assume a linear relation between precipitate radius and  $\delta$ , necessitating a scalar correction factor ( $f$ ).

A <sup>[2]</sup>	B <sup>[2]</sup>	E <sup>[3]</sup>	E <sub>2</sub> <sup>[3]</sup>	f
Energy well depth	Atom spacing at U = 0	1 <sup>st</sup> -order Young's modulus, Fe	2 <sup>nd</sup> -order Young's modulus, Fe	Linear fit parameter
0.7064 eV	2.02E-10 m	230 GPa	275 GPa	0.0037

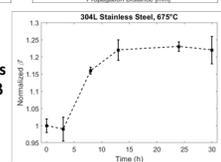
### Nonlinear Ultrasound

As an ultrasonic wave interacts with microstructural damage in a material, it generates harmonics of the original wave.  $\beta$  is quantified as:

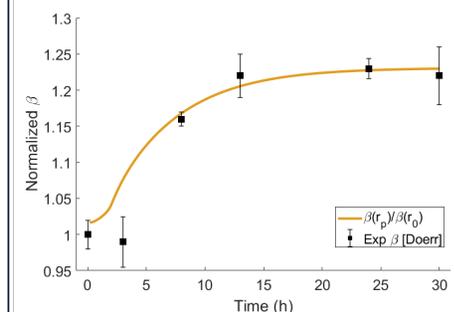
$$\beta \propto \frac{A_2}{A_1^2 x}$$



Measurements of thermally aged stainless steel specimens show a significant change in  $\beta$  with increasing time. [Doerr]



## Results



The prediction of the 1D model follows experimental data between 8 and 30 hours of aging, [Doerr] coinciding with predicted mean precipitate radii of 5 – 7 nm.

## Conclusions

A model describing evolution of acoustic nonlinearity of sensitized stainless steel 304L was developed. This model relates the radius of grain boundary  $M_{23}C_6$  precipitates to the increase in  $\beta$ , demonstrating a linear relationship over a range of precipitate radii.

## Future Work

- Assess the Lennard-Jones potential in the description of grain boundary energy.
- Determine the influence of precipitate distribution on  $\beta$
- Optimize the correction factor and determine its order across alloys.
- Use SEM or other characterization to assess the accuracy of the ThermoCalc software in the growth of grain boundary precipitates.
- Further tests on 304L stainless steel to assess repeatability and reliability of measurement.

## Reference

- [1] C Doerr, J-Y Kim, P Singh, J Wall, L Jacobs, *NDT&E Int.*, 88, p. 17-23 (2017)
- [2] V Filipova, E Blianova, N Shurygina, *Inorg. Mat. Appl. Rsch.*, 6, p. 402-406 (2015)
- [3] C Cube, J Turner, *J. Acoust. Soc. Am.*, 138, p. 2613-2625 (2015)
- [4] TC-PRISMA, <https://www.thermocalc.com/>

## Slide 1

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**J.-Y. Kim1** in Thermo-Calc

Software

Jin-Yeon Kim, 7/2/2019

**J.-Y. Kim2** Quantify degree of sensitization (DOS) using measured acoustic nonlinearity parameter

Brian, this will be the ultimate goal of the research!

Jin-Yeon Kim, 7/2/2019

**M23C6 precipitates well before sigma phase**  
[https://inis.iaea.org/collection/NCLCollectionStore/\\_Public/36/083/36083651.pdf?r=1&r=1](https://inis.iaea.org/collection/NCLCollectionStore/_Public/36/083/36083651.pdf?r=1&r=1)