

#11) Ignore wetting, ignore fiber elasticity

$$\text{So Permeability} = S = \frac{r_f^2}{4k} \frac{(1-v_f)^3}{v_c^2}$$
$$= \frac{(4 \times 10^{-6})^2}{4 \times 0.7} \frac{(1-0.64)^3}{(0.64)^2} = 6.57 \times 10^{-13} \text{ m}^2$$

velocity (from Darcy's law)

$$v = \frac{-S}{\eta} \frac{dP}{dz}$$

$$\eta = 8 \text{ Poise}$$

$$\frac{dP}{dz} \approx \frac{F/A}{dz}$$

$$F = 51b = 22.9 \text{ N, both sides} \quad \begin{array}{c} 10 \\ \downarrow \\ 5 \end{array} \quad \text{so } F = 44.8 \text{ N}$$

$$dz = 0.01 \text{ in} = 2.54 \times 10^{-4} \text{ m}$$

$$L = \frac{1}{2} \times \text{circumference} = \frac{1}{2} \times 18 \times \pi = 0.72 \text{ m}$$

$$W = \frac{1}{2}'' = 12.7 \times 10^{-3} \text{ m}$$

Assume the fibers are well distributed, so  
 $A = L_{\text{tow}} \times W_{\text{tow}}$  (sort of like a "solid")

$$A = 0.72 \times 12.7 \times 10^{-3} = 9.14 \times 10^{-3} \text{ m}$$

$$\frac{dP}{dz} = \frac{44.8}{\frac{9.14 \times 10^{-3}}{2.54 \times 10^{-4}}} = 19.3 \times 10^6 \text{ Pa/m}$$

$$v = \frac{-\Delta}{\eta} \frac{dP}{dz} = \frac{-6.51 \times 10^{-13}}{0.8} \times 19.3 \times 10^6$$
$$= 1.57 \times 10^{-5} \text{ m/s}$$

now, it has to move 0.254 mm

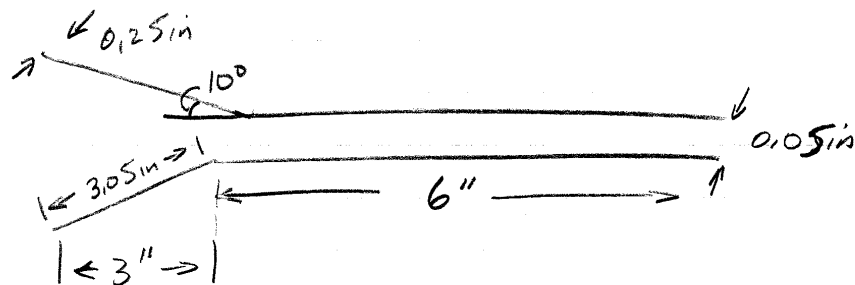
$$\text{so } t = \frac{z^2}{2} \frac{\eta}{S} \frac{1}{\Delta P} = \frac{(2.54 \times 10^{-4})^2}{2} \frac{0.8}{6.51 \times 10^{-13}} \times \frac{9.14 \times 10^{-3}}{44.8} = 8.1 \text{ s}$$

so, the fibers would need to be under pressure for at least 8s to wet out.  
so we'd need about  $\frac{1}{2}$  revolution per 8sec  
or  $3\frac{3}{4}$  rpm

#12] The starting equation is (ignoring friction):

$$\frac{1}{2(w(x)+t(x))} \frac{dF}{dx} = \eta \frac{V(x)}{t(x)} - (P + \sigma' \cos \phi) \sin \phi$$

The die looks like



First we need to determine where the bundle of fibers hits the taper. We do this from the initial and final volume fractions. If we assume the pulsation fills the die, and it is 60% by volume fibers

Assuming unit length

$$\text{Die area} = 0.125 \times 0.105 = 1.25 \times 10^{-2} \text{ in}^2$$

$$\text{Die area} \times v_f = 1.25 \times 10^{-2} \times 0.6 = 7.5 \times 10^{-3} \text{ in}^2$$

$$\text{so \# of fibers} = \frac{\text{Area of fibers}}{\text{Area of one fiber}}$$

$$\text{Area of one fiber} = \pi r^2 = \pi \times (10 \times 10^{-6})^2 = 3.14 \times 10^{-10} \text{ m}^2$$

$$\text{So, the number of fibers} = \frac{7.5 \times 10^{-3} \times 6.75 \times 10^{-4} \text{ (conversion factor)}}{3.14 \times 10^{-10}}$$

$$= 15,398 \text{ fibers}$$

Now, the area at  $v_f = 0.5$  (the starting point)

$$A = \frac{\text{Fiber area}}{v_f} = \frac{15,398 \times 3.14 \times 10^{-10}}{0.5}$$

$$A = 9.67 \times 10^{-6} \text{ m}^2$$

which gives a thickness of

$$A = w \times t$$

$$t = \frac{A}{w} = \frac{9.67 \times 10^{-6}}{6.35 \times 10^{-3}} = 1.52 \times 10^{-3} \text{ m}$$

From this we can calculate the average thickness

$$\bar{t} = \frac{t_{\max} + t_{\min}}{2} = \frac{1.52 + 1.27}{2} = 1.4 \text{ mm}$$

$$\text{how } \sigma' = \frac{3\pi E}{\beta^4} \frac{1 - \sqrt{\frac{v_f}{v_0}}}{\left(\sqrt{\frac{v_a}{v_0}} - 1\right)^4}$$

$$E = 10.5 \times 10^6 \text{ psi} = 73.4 \times 10^9 \text{ Pa}$$

$$v_a = 0.785; \quad v_o = 0.5; \quad v_f = 0.6$$

$$\beta = 220$$

we'll use an average volume fraction

$$\bar{v} = \frac{v_o + v_f}{2} = \frac{0.5 + 0.6}{2} = 0.55$$

$$\text{so } \sigma' = \frac{3 \times \pi \times 73.4 \times 10^9}{220^4} \frac{1 - \sqrt{\frac{0.55}{0.5}}}{\left( \sqrt{\frac{0.785}{0.55}} - 1 \right)^4}$$

$$= -10,031 \text{ Pa} \quad \text{opposes pulling}$$

now, to find  $P$ , we need first to get the permeability

$$S = \frac{r_f^2}{4k} \frac{(1 - v_f)^3}{v_f^2}$$

assuming  $k=1$  and an axial flow, and  $\bar{v} = 0.55$

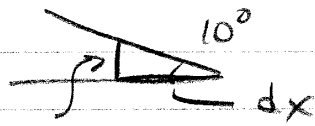
$$S = \frac{(10 \times 10^{-6})^2}{4 \times 1} \frac{(1 - 0.55)^3}{(0.55)^2}$$

$$= 7.53 \times 10^{-12} \text{ m}^2$$

now 
$$v = \frac{-s}{\eta} \frac{dP}{dx}$$

we need  $v$  to be approximately the velocity into the die or 10 mm/s

$dx$  is approximately the length in the axial direction of taper contact



$$\frac{1.52 - 1.27}{2} = 0.13 \text{ mm}$$

$$dx = 0.74 \text{ mm}$$

$$\text{so } dP \approx \frac{-v \eta dx}{s} = \frac{10 \times 10^{-3} \times 0.3 \times 0.74 \times 10^{-3}}{7.53 \times 10^{-12}}$$

$$= -2.95 \text{ kPa} \quad (\text{opposes pulling})$$

so putting together in the following equation

$$dF = 2 \bar{w} \bar{t} dx \left[ \eta \frac{v}{t} - (P + \sigma' \cos \phi) \sin \phi \right]$$

$$= 2 \times (6.35 \times 10^{-3} + 1.54 \times 10^{-3}) (0.74 \times 10^{-3}) \left[ 0.3 \frac{10 \times 10^{-3}}{1.4 \times 10^{-3}} \right]$$

$$- (-2.95 \times 10^3 + -10 \times 10^3 \cos 10) \sin 10$$

$$\text{so } df = 0.03 \cdot N = 0.0116f = 0.190z$$

not a very big number

Real numbers would make the value bigger, but it's so small to start, it wouldn't make much of a difference

This of course ignores the friction in the die, this would be a big number